

## BAB XII

### PERHITUNGAN PONDASI TELAPAK PT

#### 12.1 Beban yang Bekerja ( ETABS )

$$P_u := 8736.44 \text{ kg}$$

#### 12.2 Kontrol dimensi pondasi

##### Dimensi pondasi

$$B := 120 \text{ cm} \quad L := 120 \text{ cm}$$

$$A := B \cdot L = 14400 \text{ cm}^2$$

$$W_x := \frac{B \cdot L^2}{6} = 288000 \text{ cm}^3$$

$$W_y := \frac{L \cdot B^2}{6} = 288000 \text{ cm}^3$$

##### Tegangan yang terjadi

$$\sigma_{\max} := \frac{P_u}{A} = 0.607 \text{ kg/cm}^2$$

##### Tegangan ijin tanah ( data sondir kedalaman 1.5 m )

$$q_c := 4 \text{ kg/cm}^2$$

$$SF := 3$$

$$q_{ijin} := \frac{q_c}{SF} = 1.333 \text{ kg/cm}^2 > \sigma_{\max} = 0.607 \text{ kg/cm}^2 \quad \text{OK!!}$$

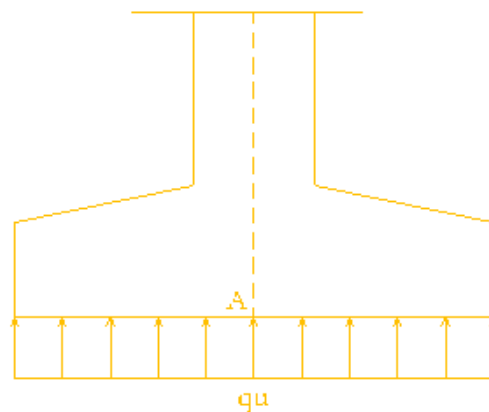
#### 12.3 Penulangan Pondasi telapak

##### Momen pada pondasi ( momen pada POT. A ) :

$$q_u := \sigma_{\max} \cdot 1000 = 606.697 \text{ kg/m}$$

$$M_p := \frac{q_u \cdot 1.2^2}{2} = 436.822 \text{ kgm}$$

$$M_{ult} := 1.2 \cdot M_p = 524.186 \text{ kgm}$$



Adapun data - data perencanaan untuk penulangan pondasi :

- Tebal pelat :  $h := 350 \text{ mm}$
- Tebal decking  $s := 50 \text{ mm}$
- Diameter tulangan rencana D13

- Mutu tulangan baja  $f_y := 390 \text{ Mpa}$
- Mutu beton  $f_c := 18.675 \text{ Mpa}$

$$\text{daksen} := 50 + 6.5 = 56.5 \text{ mm}$$

$$d := h - \text{daksen} = 293.5 \text{ mm}$$

$$b := 1200 \text{ mm}$$

$$\beta := 0.85$$

Berdasarkan SNI 2847 pasal 10.4.3 :

$$\rho_{\text{balance}} := \frac{0.85 \cdot \beta \cdot f_c \cdot \left( \frac{600}{600 + f_y} \right)}{f_y} = 0.021$$

$$\rho_{\text{max}} := 0.75 \cdot \rho_{\text{balance}} = 0.016$$

Berdasarkan SNI 03-2847-2002 pasal 9.12.2

$$\rho_{\text{min}} := \frac{1.4}{f_y} = 0.0036$$

$$m := \frac{f_y}{0.85 \cdot f_c} = 24.569$$

$$M_n := \frac{\text{Mult} \cdot 9.81 \cdot 1000}{0.8} = 6427835.73 \text{ Nmm}$$

$$R_n := \frac{M_n}{b \cdot d^2} = 0.062 \text{ N/mm}^2$$

$$\rho := \frac{\left( 1 - \sqrt{1 - \frac{2m \cdot R_n}{f_y}} \right)}{m} = 0.00016$$

$$\rho = 0.00016 < \rho_{\text{min}} = 0.0036$$

$$\text{Asperlu} := \rho_{\text{min}} \cdot b \cdot d = 1021.38 \text{ mm}^2$$

jadi pasang tulangan lentur D13-150

$$\text{Aspsg} := 9 \cdot 0.785 \cdot 13^2 = 1193.985 \text{ mm}^2$$

## 12.4 Kontrol geser pons

- Beban Aksial Kolom

Perencanaan penampang akibat geser didasarkan pada beban aksial kolom

$$N_{uk} := 259.429 \text{ kN}$$

- Dengan persyaratan  $V_u < V_c$  ( gaya geser ultimate harus lebih kecil dari kuat geser nominalnya ).

$$\text{tebal pondasi } t_p := 35 \text{ mm}$$

$$\text{dimensi kolom } 35/35 \text{ cm}$$

$$b_o := 0.5 \cdot t_p + 35 + 0.5 \cdot t_p = 70 \text{ cm}$$

$$d_o := 0.5 \cdot t_p + 35 + 0.5 \cdot t_p = 70 \text{ cm}$$

- Keliling Kritis

$$U := 2 \cdot (b_o + d_o) = 280 \text{ cm}$$

- Luas Kritis

$$A_k := U \cdot t_p = 9800 \text{ cm}^2$$

- Kekutan Geser Beton

$$\beta_c := \frac{35}{35} = 1$$

$$d := t_p - 5 - 1.3 = 28.7 \text{ cm}$$

$$V_c := \frac{\sqrt{f_c} \cdot U \cdot d \cdot 100 \cdot \left( 1 + \frac{\beta_c}{2} \right)}{6 \cdot 10^3} = 868.181 \text{ kN} \quad \text{..... SNI 2847 pasal 13.12.2.1}$$

Syarat  $V_u \leq \phi V_c$

$$\phi := 0.75$$

$$N_{uk} = 259.429 \text{ kN} \quad \blacksquare < \blacksquare \quad \phi \cdot V_c = 651.136 \text{ kN} \quad \text{..... OK!!!}$$

